

**MULTIPLE CHOICE PROBLEMS (10 Points each)**

1. In the hanger shown, the upper portion of link  $ABC$  is  $3/8$  in. thick and the lower portions are each  $1/4$  in. thick. Epoxy resin is used to bond the upper and lower portions together at  $B$ . The pin at  $A$  is of  $3/8$  in. diameter. The shearing stress in pin  $A$  is most nearly

- (a) 6790 psi  
 (b) 3400 psi  
 (c) 2530 psi  
 (d) 1260 psi  
 (e) 1070 psi

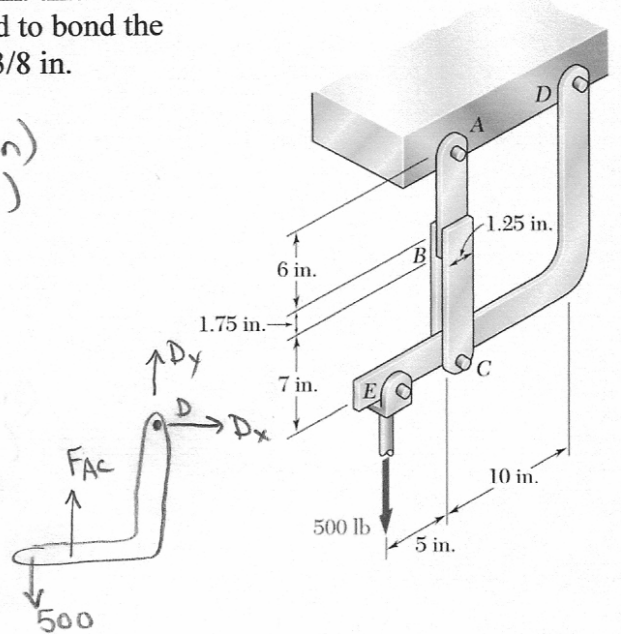
$$\sum M_D = 0 = (500 \text{ lb})(15 \text{ in}) - F_{AC}(10 \text{ in})$$

$$F_{AC} = 750 \text{ lb}$$

$$\tau_A = \frac{F_{AC}}{A_{\text{pin}}}$$

$$= \frac{750 \text{ lb}}{\frac{\pi}{4} \left(\frac{3}{8} \text{ in}\right)^2}$$

$$= \underline{\underline{6790 \text{ psi}}}$$



2. A couple  $M$  of magnitude  $1500 \text{ N}\cdot\text{m}$  is applied to the crank of an engine. For the position shown, the average normal stress in connecting rod  $BC$  which has a  $450\text{-mm}^2$  uniform cross section is most nearly

- (a) -20.7 MPa  
 (b) -41.4 MPa  
 (c) -3.33 MPa  
 (d) -6.66 MPa  
 (e) -10.4 MPa

$$\vec{F}_{BC} = -F_{BC} \frac{60}{200} \hat{i} - F_{BC} \frac{200}{200} \hat{j}$$

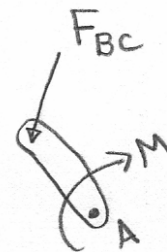
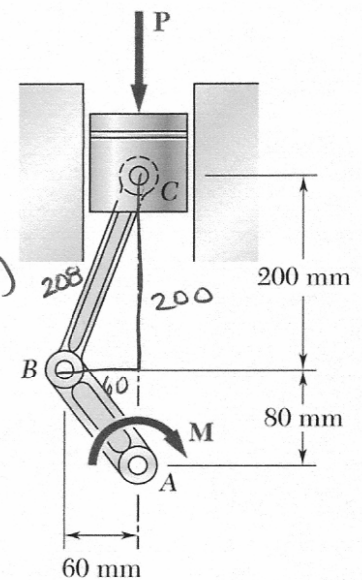
$$\sum M_A = 0 = -M + F_{BC} \frac{60}{200} (0.08 \text{ m}) + F_{BC} \frac{200}{200} (0.06 \text{ m})$$

$$F_{BC} = 18.64 \text{ kN}$$

$$\sigma_{BC} = -\frac{F_{BC}}{A_{BC}}$$

$$= -\frac{18.64 \text{ kN}}{450 \text{ mm}^2}$$

$$= \underline{\underline{-41.4 \text{ MPa}}}$$



3. The plastic block shown is bonded to a rigid support and to a vertical plate to which a 240-kN load  $P$  is applied. If the plastic has a shear modulus of 1050 MPa, the deflection of the plate is most nearly

- (a) 18.29 mm  
 (b) 6.86 mm  
 (c) 11.43 mm  
 (d) 2.86 mm  
 (e) 1.190 mm

$$\tau = \frac{P}{(80\text{mm})(120\text{mm})}$$

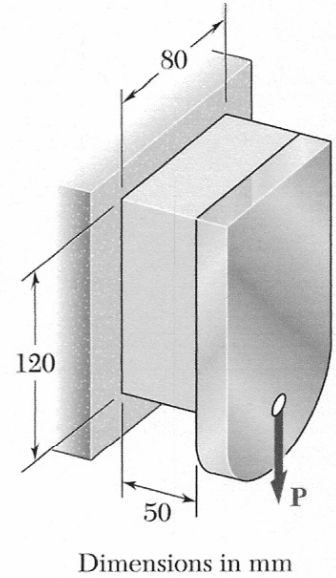
$$= \frac{240 \times 10^3 \text{ N}}{9600 \text{ mm}^2}$$

$$= 25 \text{ MPa}$$

$$\gamma = \frac{\tau}{G} = \frac{\delta}{50\text{mm}}$$



$$\delta = \frac{\tau}{G} (50\text{mm}) = \frac{25 \text{ MPa}}{1050 \text{ MPa}} (50\text{mm}) = \underline{\underline{1.190 \text{ mm}}}$$



4. Knowing that  $\sigma_{ult} = 240 \text{ MPa}$ , and that a factor of safety of 2.0 is required, the maximum allowable value of the centric axial load  $P$  is most nearly

- (a) 54.3 kN  
 (b) 41.7 kN  
 (c) 143.9 kN  
 (d) 90.0 kN  
 (e) 35.3 kN

@ A  $d = 80 \text{ mm}$

$$r = 10 \text{ mm}$$

$$\frac{r}{d} = 0.125$$

$$K = 2.65$$

$$P_{all} = \frac{(120 \text{ N/mm}^2)(15 \text{ mm})(80 \text{ mm})}{2.65}$$

$$= \underline{\underline{54.3 \text{ kN}}}$$

$$\sigma_{all} = \sigma_{ult} / FS$$

$$= 240 / 2 = \underline{\underline{120 \text{ MPa}}}$$

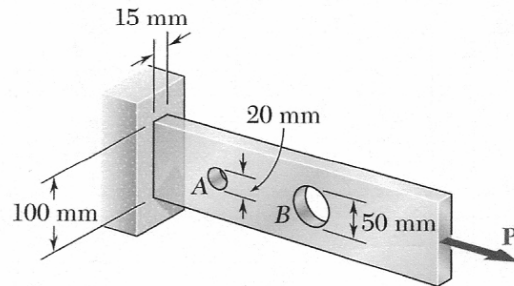
@ B  $d = 50 \text{ mm}$

$$r = 25 \text{ mm}$$

$$\frac{r}{d} = 1/2$$

$$K = 2.16$$

$$P_{all} = \frac{(120 \text{ N/mm}^2)(15 \text{ mm})(50 \text{ mm})}{2.16} = \underline{\underline{41.7 \text{ kN}}}$$



5. An aluminum wire having a diameter  $d = 2$  mm and length  $L = 3.8$  m is subjected to a tensile load  $P$  (see figure). The aluminum has a modulus of elasticity  $E = 75$  GPa. If the maximum permissible elongation of the wire is 3.0 mm and the allowable stress in tension is 60 MPa, the allowable load  $P_{max}$  is most nearly

(a) 189 N

(b) 186 N

(c) 183 N

(d) 180 N

(e) 177 N

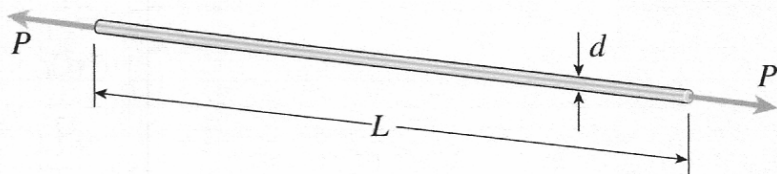
$$\delta = \frac{PL}{AE}$$

$$P_{max} = \frac{\delta AE}{L}$$

$$= \frac{(0.003 \text{ m}) \frac{\pi}{4} (0.002 \text{ m})^2 (75 \times 10^9 \text{ N/m}^2)}{3.8 \text{ m}} = \underline{\underline{186 \text{ N}}}$$

$$\sigma = \frac{P}{A}$$

$$P_{max} = \sigma_{all} A = (60 \times 10^6 \text{ N/m}^2) \left( \frac{\pi}{4} \right) (0.002 \text{ m})^2 = \underline{\underline{188.5 \text{ N}}}$$



6. A line of slope 4:10 has been scribed on a cold-rolled yellow-brass plate, 6 in. wide and 0.25 in. thick. For this material,  $E = 15 \times 10^6$  psi and  $\nu = 0.34$ . The slope of the line when a 45-kip compressive centric axial load is applied is most nearly

(a) 3.99728:10.02 (0.39893)

(b) 6:8 (0.75)

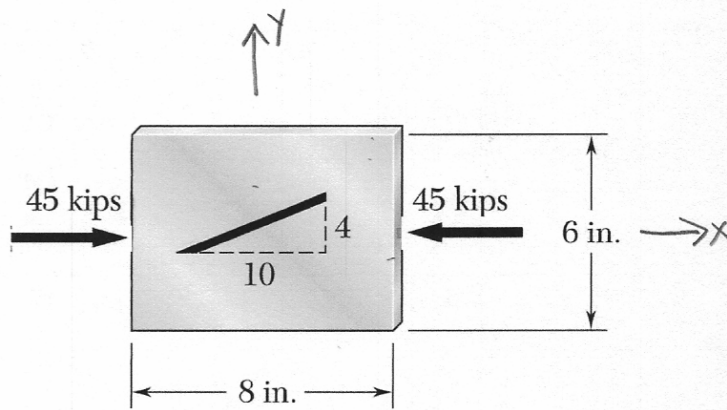
(c) 4.99592:8.016 (0.62324)

(d) 4.00272:10.02 (0.39947)

(e) 4.00272:9.98 (0.40107)

$$\sigma_x = \frac{P}{A}$$

$$= \frac{45 \text{ kips}}{(6 \text{ in})(0.25 \text{ in})} = \underline{\underline{-30 \text{ ksi}}}$$



$$\epsilon_x = \frac{1}{E} \sigma_x = \frac{-30 \times 10^3 \text{ psi}}{15 \times 10^6 \text{ psi}} = -0.002$$

$$\epsilon_y = -\frac{\nu}{E} \sigma_x = -\frac{0.34}{15 \times 10^6 \text{ psi}} (-30 \times 10^3 \text{ psi}) = +6.8 \times 10^{-4}$$

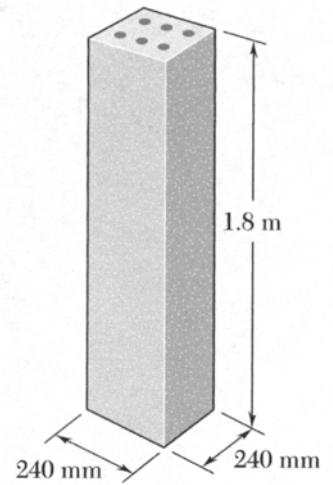
$$L'_x = L_x (1 + \epsilon_x) = 10 (1 - 0.002) = 9.98$$

$$L'_y = L_y (1 + \epsilon_y) = 4 (1 + 6.8 \times 10^{-4}) = 4.00272$$

**WORK OUT PROBLEM (40 Points)**

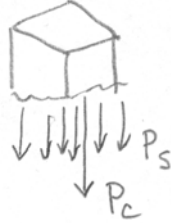
7. The concrete post ( $E_c = 25 \text{ GPa}$  and  $\alpha_c = 9.9 \times 10^{-6} / ^\circ\text{C}$ ) is reinforced with six steel bars, each of 22-mm diameter ( $E_s = 200 \text{ GPa}$  and  $\alpha_s = 11.7 \times 10^{-6} / ^\circ\text{C}$ ). If the temperature increases  $35^\circ\text{C}$ , determine

- (a) the normal stresses induced in the steel,  
 (b) the normal stresses induced in the concrete.



Equilibrium

$$P_c + 6P_s = 0$$



Load-Temperature-Deformation

$$\delta_c = \frac{P_c L}{A_c E_c} + \alpha_c \Delta T L$$

$$\delta_s = \frac{P_s L}{A_s E_s} + \alpha_s \Delta T L$$

Kinematics

$$\delta_c = \delta_s$$

$$\frac{P_c L}{A_c E_c} + \alpha_c \Delta T L = \frac{P_s L}{A_s E_s} + \alpha_s \Delta T L$$

$$(\alpha_c - \alpha_s) \Delta T = \frac{P_s}{A_s E_s} + \frac{6P_s}{A_c E_c} = P_s \left( \frac{1}{A_s E_s} + \frac{6}{A_c E_c} \right)$$

$$P_s = \frac{(\alpha_c - \alpha_s) \Delta T}{\frac{1}{A_s E_s} + \frac{6}{A_c E_c}}$$

$$= \frac{(9.9 \times 10^{-6} / ^\circ\text{C} - 11.7 \times 10^{-6} / ^\circ\text{C})(35^\circ\text{C})}{\frac{1}{\frac{\pi}{4}(22\text{mm})^2(200 \times 10^3 \text{N/mm}^2)} + \frac{6}{[(240\text{mm})^2 - 6 \cdot \frac{\pi}{4}(22\text{mm})^2](25 \times 10^3 \text{N/mm}^2)}}$$

$$= \frac{1}{\frac{\pi}{4}(22\text{mm})^2(200 \times 10^3 \text{N/mm}^2)} + \frac{6}{[(240\text{mm})^2 - 6 \cdot \frac{\pi}{4}(22\text{mm})^2](25 \times 10^3 \text{N/mm}^2)}$$

$$= -3600 \text{ N}$$

(a)  $\sigma_s = \frac{P_s}{A_s}$   
 $= \frac{-3600 \text{ N}}{\frac{\pi}{4}(22\text{mm})^2}$   
 $= -9.47 \text{ MPa}$

(b)  $P_c = -6P_s = -21600 \text{ N}$   
 $\sigma_c = \frac{P_c}{A_c} = 0.391 \text{ MPa}$

